

# Counter-Rotating Gyres as a Non-Local Effect of Resonating Basin Modes

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Relatively high Reynolds number calculations of a barotropic ocean model reveal counterrotating gyres on the eastern side of the basin. These unintuitive regions rotate in a direction opposite to the wind forcing direction, and are sometimes associated with strong up-gradient vorticity fluxes. An analysis of the empirical orthogonal functions of some numerical calculations reveals that much of the variance is in oscillations resembling basin modes. A simple non-local model of the nonlinear interaction of forced-dissipative basin modes, together with the observed variance of each mode in the numerical calculation, gives excellent agreement with the streamfunction and dynamical balances of the counter-rotating gyres.

(Fox-Kemper, 2003)

The model results presented here are from a 257x257 Chebyshev polynomial pseudo-spectral numerical barotropic model in a rectangular basin with spatially-variable viscosity to roughly parameterize boundary physics not directly represented in the model. The nondimensional equations governing the model are:

$$\begin{split} \frac{\partial \zeta}{\partial t} + \nabla \cdot (\hat{\mathbf{x}}\psi + \delta_I^2 \mathbf{u}\zeta - \delta_M^3 \nabla \zeta + \delta_S \nabla \psi) &= -\sin(\pi y), \\ \zeta &= \nabla^2 \psi, \\ \delta_M^3 &= \frac{\delta_I^3}{\mathrm{Re}_{\mathrm{i}}} + \left(\frac{\delta_I^3}{\mathrm{Re}_{\mathrm{b}}} - \frac{\delta_I^3}{\mathrm{Re}_{\mathrm{i}}}\right) \left(e^{-x/\delta_d} + e^{-(1-x)/\delta_d}\right), \\ \delta_d &\equiv \frac{\delta_I}{\sqrt{\mathrm{Re}_{\mathrm{i}}}}, \end{split}$$

where  $\psi$  (streamfunction) and  $\zeta$  (relative vorticity) are determined during integration. Boundary conditions are slip ( $\zeta = 0$ ) on the 'fluid' boundaries and no-slip ( $\frac{\partial \psi}{\partial x} = 0$ ) on the 'solid' boundaries, as well as impermeability on all boundaries ( $\psi = 0$ ). The basin domain is y between 0 and 1 and x between 0 and  $x_e$ . The other parameters are  $\delta_I$  (Charney, 1955, inertial boundary layer width),  $\delta_S$  (Stommel, 1948, frictional boundary layer width), and Re<sub>i</sub> and Re<sub>b</sub> are Reynolds numbers for the interior and boundary viscosity (Munk, 1950). Throughout,  $\delta_I$  is 0.02 and  $\delta_S$  is 0, while Re<sub>i</sub> and Re<sub>b</sub> vary.

#### III.a. Counter-Rotating Gyres

The enhanced viscosity near the boundary allows for much higher interior Reynolds number without inertial domination (Fox-Kemper and Pedlosky, 2003).



The time-mean streamfunction for a number of parameter settings shows regions rotating counter to the wind stress.

#### III.b. Resonating Basin Modes



The  $\psi$  EOFs and PSDs of EOF presence for a  $Re_b$ =0.25,  $Re_i$ =5 calculation.



The  $\zeta$  EOFs and PSDs of EOF presence for a  $Re_b$ =0.25,  $Re_i$ =5 calculation.



The  $\psi$  EOFs and PSDs of EOF presence for a Re<sub>b</sub>=1, Re<sub>i</sub>=1 calculation in an elongated basin.

### Abstract

## II. Model

(1)
(2)
(3)

(4)







Counter-rotating gyres in other models have been attributed to Fofonoff (1954) gyres (predicted by inviscid statistical mechanics Griffa and Castellari, 1991; Özgökmen and Chassignet, 1998), mixing of absolute vorticity (Greatbatch and Nadiga, 1999), and nonlinear dispersion (Holm and Nadiga, 2003). However, the Fofonoff (1954) primary is mean vorticity advection and  $\beta$ -term; some regions would require 'up-gradient' absolute vorticity fluxes; and the gyres have a sensitive dependence on the frequency of the boundary current instabilities not captured by the dispersion model.

In summary,

- EOFs strongly resemble spatial structure of basin mode standing waves with two EOFs per basin mode.
- PSDs of EOF presence have peaks at basin mode frequencies.
- Vorticity EOFs reveal that most variance in in boundary current region, but frequency matches that of the resonating modes.
- Thus, there are basin modes forced by boundary current instabilities.
- The counter-rotating gyres occur on the eastern side, where basin modes are the most important variability, and their vorticity balance depends critically on eddy flux divergences.

Consider a grossly simplified model, replacing Laplacian friction with bottom drag and representing the boundary mode instabilities as an additional forcing.

$$\frac{\partial \nabla^2 \psi}{\partial t} + \frac{\partial \psi}{\partial x} + \delta_I^2 J(\psi, \nabla^2 \psi) + \delta_S \nabla^2 \psi = -\sin(\pi y) + A_f \sin(n_f \pi y) \cos(\omega_f t) e^{-x/\delta_f}.$$
 (5)

Consider the weakly nonlinear perturbation series:  $\psi = \psi_0 + \epsilon \psi_1 + \ldots$  under the assumption that  $\delta_I \ll 1$ . The  $\psi_0$  equation is linear, so it is uncoupled into a steady equation (similar to Stommel (1948)) and a time-dependent equation (similar to Pedlosky, 1965). By differentiating the linear solutions, the first nonlinear correction can be calculated. If the periodic forcing is resonant with a basin mode, then the results are to lowest order in  $\delta_S$ :

$$\delta_I^2 J(\overline{\psi_0}, \nabla^2 \overline{\psi_0}) \approx \frac{1}{2} \pi^3 \delta_S \delta_I^2 \sin(2\pi y), \tag{6}$$

$$\delta_I^2 \overline{J(\psi_0', \nabla^2 \psi_0')} \approx \frac{2m^3 n_f \pi^4 \omega_f^4 |\varphi_0|^2 \delta_I^2}{\delta_S^2} \sin(2m\pi x) \sin(2n_f \pi y) \left(1 - 2(-1)^m e^{-\frac{1}{\delta_f}} \cos\left(\frac{1}{2\omega_f}\right) + e^{-\frac{2}{\delta_f}}\right).$$

The resulting mean vorticity flux convergence is very large within the western boundary current but  $O(\delta_S \delta_I^2)$  outside it. On the other hand, the eddy term is  $O(|\varphi_0|^2 \delta_I^2 / \delta_S^2)$  outside of the forcing region. The analytic eddy flux divergence gives approximate nonlinear interaction outside of the boundary current region, resulting in a correction to Sverdrup flow.

$$\overline{\psi_0} + \overline{\psi_1} = (1-x)\sin(\pi y) + \int_1^x \delta_I^2 \overline{J(\psi_0', \nabla^2 \psi_0')} \mathrm{dx}.$$
(7)

Although the strength of each basin mode depends in a complicated way on the boundary current instabilities, the eddy interaction as a function of the average variance of the basin mode, which we can deduce from the EOFs.

$$\delta_I^2 \overline{J(\psi_0', \nabla^2 \psi_0')} \approx 4\pi^4 m n_f (m^2 + n_f^2) \delta_I^2 \sin(2m\pi x) \sin(2n_f \pi y) \int_0^1 \int_0^1 \overline{(\psi_0')^2} dx dy, \qquad (8)$$



(a) and (b) show the meridional and zonal averages, respectively, of terms in (5) in the region where  $\overline{\psi}$  < 0 (the counterrotating gyre) from the Rei=Reb=3 elongated basin calculation with wind only in the western half of the basin.

# IV. Theory

The variances of a few basin modes are deduced from the EOFs of a model calculation. The nonlinear interaction of the *analytic* basin modes produces good agreement with the interior solution, including the counter-rotating regions.



a) The time-mean streamfunction in a elongated basin with  $Re_b=3$ ,  $Re_i=3$ . There is wind forcing only in the western half of the basin. b) The prediction with analytic basin modes (3,1), (2,1), (1,2), (1,1), and (2,2) with variances from EOF diagnosis.

- Basin modes dominate the variability of the basin interior.
- gives good agreement for deviations from Sverdrup (1947) interior flow.

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linearity.

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### V. Confirmation of Theory





a) The time-mean streamfunction minus the Sverdrup (1947) interior solution for the  $Re_b$ = 0.25,  $Re_i$ = 5 calculation reveals a counter-rotating and co-rotating gyre pattern irreconcilable with a local downgradient absolute vorticity flux. b) The prediction using basin modes (1,1), (1,2), (2,1), and (2,2) with variances from EOF diagnosis.

# VI. Conclusions

• These basin modes resonate and are forced by instabilities of the western boundary current. • In the basin interior, basin modes, not vortices or mean-mean interaction dominates the non-

• Calculating the nonlinear interaction of analytic basin modes with the variances from EOFs

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